ORIGINAL RESEARCH



Comparison of various controller design for the speed control of DC motors used in two wheeled mobile robots

Huma Khan¹ · Shahida Khatoon¹ · Prerna Gaur²

Received: 12 December 2019/Accepted: 17 November 2020/Published online: 2 January 2021 © Bharati Vidyapeeth's Institute of Computer Applications and Management 2021

Abstract This work describes the study of modeling and controller on wheeled mobile robots designed the motors which is driving the wheels. According to the structure and design of wheeled mobile robot, DC motors are the best suited for the motion control. The kinematical model is required for the designing process of the wheels in the WMR. The analysis of the mathematical model is divided into angle and velocity of the dc motor build in wheeled mobile robot because of the importance of motor parameters for stability. The main focus of the work is to develop an efficient controller to control the speed of the dc motor applied in the wheels of the robot. PID tuning has been implemented in designing of the controller for the speed control of dc motor. The open loop and closed loop performance of a two wheeled mobile robot with PID and LQR controllers are obtained and compared by using MATLAB programs and simulations.

Keywords Kinematic model \cdot Controller design \cdot PID \cdot LQR \cdot Speed control \cdot DC motor \cdot Two wheeled mobile robot \cdot MATLAB simulation

Huma Khan humazakhan@yahoo.com

Shahida Khatoon skhatoon@jmi.ac.in

Prerna Gaur prernagaur@yahoo.com

¹ Department of Electrical Engineering, Jamia Millia Islamia, New Delhi, India

² Division of ICE, NSUT, New Delhi, India

1 Introduction

Mobile robots are seems to be everywhere in today's scenario and are used in huge variety of applications. The work of mobile robot is to give the command to finish the operation or any task. Legged robots design and control is complicated in comparison to the wheeled mobile robots. Robot motion is alteration or refashioning of awareness of the elements of physical environment.

Two wheeled mobile robots are more beneficial in comparison to other mobile robots and easily controllable in comparison to the legged robots. The appropriate analysis of parameters is required for the control of motion which includes the derivation of kinematic model to study the behavior of mechanical system. Since the wheels of mobile robot directly influence the movement of the robot. We can generate free paths through road map or cell decomposition in accustomed environment. Robot should have a very important feature which can adapt its characteristic to handle any type of situation.

The document mainly focuses on the velocity control of dc motor applied in the wheels of the two wheeled mobile robot. The TWMR has been assembled with the wheels and controller which is consists of motor, driver and controller. This study presents the speed control of wheels of the mobile robot by controlling the speed of motor. First a mathematical model has been derived for a dc motor in the terms of angle and velocity of dc motor. Then simulink model of dc motor has been designed in MATLAB and its response has been modified by using various control techniques. Then the speed of the dc motor has been controlled by PID Controller and LQR (linear quadratic regulator) controller. In last section the comparison of both the techniques is presented.

2 Literature survey

The Kalman filter is used to reduce the existing excursions and for getting the angular position of the links. Input tracking can be used to catechize the interpretation of the PD-Fuzzy and PID controllers. A difference between the PD-Fuzzy and PID for the stasis control of an elongated and outstretched dual link of the TWMR has been discussed in [1, 2].

Round pipes or ducts that are usually represented by cylindrical workspace are often maintained by wheeled mobile robots (WMR). On the basis of this analysis, screw theory forms an important tool and is used to analyze the dynamic behavior of wheeled mobile robots in cylindrical workspaces.

The law of control on the basis of two axis measuring instruments facts is put forward which can lead the robot to move parallel in round pipes or ducts. Simulation of the movement of the single wheel totally scrolling in the cylindrical workspace has been done in [3-5] (Fig. 1).

Non-linear and unstable characteristics of wheeled mobile robot arises interest in researcher that intensively providing assistance to the human for performing their regular exercise or tasks, for human transportation, for teaching objective and assistance robotics [6–10]. Initially there are so many hurdles comes to designing of controller. For the solution of wheeled mobile robot control issue experiments of various controlling techniques have been done. Feedback linearization approach is also used for solving non-linear system, so that we can applied linear laws to non-linear system [11–14]. A lot of studies have been made aiming at tracking trajectories accurately, including methods of optimal control, robust control, adaptive control, back-stepping control, neural networks control and integral sliding-mode control [15–17].

This paper is organized as follows: In section III we describe the mobile robot, section IV describes controller design, and section V presents simulation results. Finally, the conclusion is presented in section VI. In this document we have designed various linear controllers for the system and applied to it. Slipping and cornering forces are considered negligible in designing mathematical modeling of wheeled mobile robot.

Mathematical Modeling.

The equivalent circuit of DC motor can be represented in electromechanical for the wheeled mobile robot case. The equivalent circuit diagram of electromechanical system of the motor is shown in Fig. 2.

 R_{eq} is the equivalent resistance and L_{eq} is the equivalent inductance of the coil of the dc motor. Torque of the motor is taken as τ and the input voltage of the dc motor has been taken as V_t .

The equations of the system are as follows:

The torque equation of dc motor in the form of armature current and the constant is:

$$\tau = K * i_a \tag{1}$$

The relationship between angular velocity ω_m and generated voltage e_a is given by

$$\mathbf{e}_{\mathbf{a}} = \mathbf{K}\omega_m = \mathbf{K}\left(\frac{\mathrm{d}\theta}{\mathrm{d}t}\right) \tag{2}$$



Fig. 1 Two wheeled dc motor assembly with wheel and controller



Fig. 2 Equivalent circuit diagram of the dc motor

By applying Kirchhoff's law and Newton's law in the Fig. 2, these expressions can be obtained.

$$J\frac{d^2\theta}{dt^2} + b\frac{d\theta}{dt} = Ki_a$$
(3)

$$L\frac{di_a}{dt} + Ri_a = V - K\frac{d\theta}{dt}$$
(4)

These equations are converted into the following equations by taking the Laplace transformation.

$$Js^{2}\theta(s) + bs\theta(s) = KI(s)$$
(5)

$$LsI(s) + RI(s) = V(s) - Ks\theta(s)$$
(6)

From (5)
$$I(s) = \frac{Js^2 + bs}{K} \theta(s)$$

As $= \omega_m = \left(\frac{d\theta}{dt}\right) > W_m(s) = s\theta(s)$
From (6) $\left(\frac{Js^2 + bs}{K} \theta(s)\right)(Ls + R) = V(s) - Ks\theta(s)$
 $\theta(s) \left[\frac{K^2 + (Ls + R)(Js^2 + bs)}{K}\right] = V(s)$

Now By solving these equations, we get

- 2 .

$$G_{p}(s) = \frac{\theta(s)}{V(s)} = \frac{K}{\left\{s\left[(R + Ls)(Js + b) + K^{2}\right]\right\}}$$
(7)

$$G_{v}(s) = \frac{w(s)}{V(s)} = \frac{K}{\{\left[(R + Ls)(Js + b) + K^{2}\right]\}}$$
(8)

For a 12 V dc motor considering the number of turns of the motor N = 5000 rpm and power is 8 watts. Let us consider the inertia of rotation is to be J = 0.01.

Then K can be calculated K as

$$\omega_{\rm m} = \frac{V_{\rm t}}{K} = \frac{2\pi N}{60} \tag{9}$$

The value of constant K is 0.023 and the angular velocity is 524 rad/s.

The calculations for the torque τ is

$$\tau = \frac{P}{W} = 15.27 \text{mNm.} \tag{10}$$

The specifications of the parameters in the dc motor of wheeled mobile robot are given in Tables 1, 2.

Table 1 Specification of the parameters of WMR

Parameter	Description	Value	Units
L	Inductance	0.5	Henry
J	Rotational Inertia	0.01	Kgm ²
В	Viscous Friction coefficient	0.00003	Nm-sec
V _t	Terminal voltage	12	Volt
K	Motor torque constant	K = 0.023	Nm/Amp
R	Terminal Resistance	1	Ω

Table 2 Comparison of parameters

OLTF	CLTF	Р	PI	PID	LQR
40.5	0.73	0.90	0.54	0.17	1.29
72.6	3.83	3.07	3.22	2.16	2.06
43.4	1.17	1.11	1.28	1.03	1.00
134.9	1.66	1.98	1.27	1.21	3.01
0	19.47	13.91	27.79	2.66	0.36
39.2	0.90	0.89	0.92	0.90	0.91
43.4	1.17	1.11	1.28	1.03	1.01
	OLTF 40.5 72.6 43.4 134.9 0 39.2 43.4	OLTF CLTF 40.5 0.73 72.6 3.83 43.4 1.17 134.9 1.66 0 19.47 39.2 0.90 43.4 1.17	OLTF CLTF P 40.5 0.73 0.90 72.6 3.83 3.07 43.4 1.17 1.11 134.9 1.66 1.98 0 19.47 13.91 39.2 0.90 0.89 43.4 1.17 1.11	OLTFCLTFPPI40.50.730.900.5472.63.833.073.2243.41.171.111.28134.91.661.981.27019.4713.9127.7939.20.900.890.9243.41.171.111.28	OLTFCLTFPPIPID40.50.730.900.540.1772.63.833.073.222.1643.41.171.111.281.03134.91.661.981.271.21019.4713.9127.792.6639.20.900.890.920.9043.41.171.111.281.03

3 Controller design

By using the overall transfer function of DC motor in terms of angle and velocity, the step response of the dc motor is shown in Fig. 3.

Settling time for open loop step response is 72.58 s. which is very large. The closed loop step response is shown in Fig. 4. Settling time for closed loop step response is 3.83 s. which yield a good result as compared to open loop transfer function but also we got overshoot here which we tries to minimize by using controller.

A. P-Controller:

Output of the proportional controller is given by the multiplication of controller gain and plant function.

$$Con(t) = k_p e(t) \tag{11}$$

Here Con (t) is the controller output.

B. PI-Controller:

Output of the proportional integral controller is given by:

$$Con(t) = k_p e(t) + K_i \int_0^T e(\tau) d\tau$$
(12)

Integral term contains product of integral gain and summation of errors. It improves the steady state response.

C. PID Controller:

Output equation is given by following equation:

$$Con(t) = k_p e(t) + K_i \int_0^T e(\tau) d\tau + K_d \frac{de(t)}{dt}$$
(13)

Here e(t) is dissimilitude of the desiderate reference points and current proportion (process variable measurement), r(t) is the input reference. k_p , K_i and K_d are proportional gain, integral gain and derivative gain respectively of a PID controller.

We have designed a PID feedback controller. The transfer function of the PID is given as



Fig. 4 The step response of

close loop dc motor



$$Cont(s) = \frac{U(s)}{E(s)} = k_p + \frac{K_i}{s}$$
(14)

$$C(s) = \frac{k_d s^2 + K_p s + K_i}{s} \tag{15}$$

D. LQR controller:

It stand for Linear Quadratic Regulator. It can be applied to linear systems or linearized non linear

systems. State-Space model of a linear system is given by following equation:

$$\dot{x} = Ax + Bu \tag{16}$$

$$y = Cx + Du \tag{17}$$

For optimal control approach, we have to find a state feedback law that minimizes the cost function given by:



controller









$$J = \frac{1}{2} \int_0^\infty (x^T Q x + U^T R U) dt$$
(18)

Here Q and R are weighting matrix which include weight on states and control input respectively.

4 Results and discussion

PID Controller has been applied to the DC motor to control the motor's speed and improving the performance. Figures 5, 6 show the model and response of PID controller applied to the DC motor and its response. Figures 7, 8 show the model and response of PID controller applied to both the motors. Figure 9 shows the linear quadratic response of the motor. The complete analysis shows that the LQR is giving better performance in comparison to PID controller. According to our design constraint with increasing value of we k_p get the oscillatory response which is not desired at all and for decreasing value of k_p settling limit is not in designing range.

E. P-Controller

Using pid tuner we get k_p =0.7482. Response under P controller is given in Fig. 5.

According to our design constraint with increasing value of k_p we get the oscillatory response which is not desired at all and for decreasing value of k_p settling limit is not in designing range.

F. PI-Controller

Best value of k_p and K_i is 1.502 and K_d is 0.06034 respectively. Response is given in Fig. 6. Here response shows oscillatory nature and peak value



Fig. 8 step response of PID controller of close loop transfer function





is also high so now we introduce D factor in it to compensate the problems encountered in PI controller.

G. PID-Controller

Again using pid tuner we get the value of gains k_p , K_i and K_d which are 5.404, 2.69 and 2.713 respectively. Response for the controller is given in Fig. 7. Close loop system and System under PID controller can be viewed in Fig. 8 simultaneously.

Robustness of system is a problem. Also we can only control one state at a time. If we want to control position as well as velocity simultaneously we will go for state feedback system.

H. LQR-Controller

Since our system is controllable so now we can design state feedback system with K i.e., gain matrix by providing a command K = lqr (A, B, Q, R). Q is selected by using y = 21 and R = 1. Response can be seen in Fig. 9

This response shows less settling time as well as less overshoot in comparison to P, PI, PID Controllers.

5 Conclusion

The mathematical model of the simplified DC motor is taken and simulated; P, PI, PID controller and a LQR have been designed for improving the performance. A differential drive wheeled robot application is presented with simulated model in simulink and in editor command window. Various controllers are designed for improving the performance. PI gives oscillatory response but PID has compensated it and provided good results. LQR yields better result as compared to all the controllers used in this work. Overall analysis shows that the LQR is giving better performance than P, PI, PID controller. It can be analyzed from the plots that system has been settled in the half of the time in comparison to the PID controller. Future work involves fuzzy controller. More number of observations is needed to be performed for the evaluation of the robustness of the system. Future work will also consider the friction on wheels as well as slippage and use of non-linear controller for designing purposes.

References

- Hafiz Muhammad YasirNaeem*, A Mahmood "Autonomous Cruise Control of Car Using LQR and H2 Control Algorithm" 978-1-4673-8753-8/16/\$31.00 ©2016 IEEE
- Ronald Ping Man Chan, Karl A. Stol, C. Roger Halkyard (2013) Review of modelling and control of two-wheeled robots Elsevier, Ann Rev Control 37: 89–103
- Xu J-X, Guo Z-Q, Lee TH (2013) Design and implementation of a Takagi-Sugeno-type fuzzy logic controller on a two-wheeled mobile robot. IEEE Trans Ind Electron 60(12):5717–5728
- 4. Miller P (2008) Building a two wheeled balancing robot. 1-120
- Khatoon S, Khan H, Gaur P (2019) PID design utilized controller for DC engine employed in wheeled in movable golem. In: 2019 international conference on "Innovative Technologies in Mechanical Engineering (ITME-2019)"
- Koo J, Choi S, Won S (2009) Observer-Based Trajectory Tracking Control for a Wheeled Mobile Robot" Proceeding of the 7th Asian Control Conference, 9, 2009. HongKong, China
- 7. Xiaokan W, Dongqing F (2008) Research of LQR controller design method based on MATLAB. Micro Computer Information 24:1–5
- Oriolo G, De Luca A, Vendittelli M (2002) "WMR control via Dynamic feedback linearization: design, implementation, and experimental validation. IEEE Trans Control Syst Technol 10(6):835–852
- Kuhne F, Lages WF, da Silva JMG Jr (2004) Model predictivecontrol of a mobile robot using linearization, Proceedings of mechatronics and robotics, 525–530

- Su KH (2012) Robust tracking control design and its application to balance a two-wheeled robot steering on a bumpy road. Proc Inst Mech Eng, Part I: J Syst Control Eng 226(7):887–903
- Chwa D (2010) Tracking control of differential-drive wheeled mobile robots using a backstepping-like feedback linearization. IEEE Trans Syst, Man, Cybernetics Part A: Syst Humans 40(6):1285–1295
- Xu JX, Guo ZQ, Lee TH (2014) Design and implementation of integral sliding-mode control on an underactuated two-wheeled mobile robot. IEEE Trans Ind Electron 61(7):3671–3681
- 13. Kamel MA, Zhang YM (2014) Developments and challenges in wheeled mobile robot control," in International Conference on Intelligent Unmanned Systems (ICIUS)
- 14. Tzafestas SG (2014) Introduction to Mobile Robot Control. Elsevier
- Al-Araji AS et al (2013) Applying posture identifier in designing an adaptive nonlinear predictive controller for nonholonomic mobile robot. Elsevier, Neurocomput 99:503–554
- Muhammad Farhan Manzoor*, Qinghe Wu and Rana Javed Masood "Coordination Control of Wheeled Mobile Robot Using MPC" 7th International Conference on Computational Intelligence, Communication Systems and Networks (CICSyN) 978-1-4673-7016-5/15 \$31.00 © 2015 IEEE
- Muhammad Farhan Manzoor* and Qinghe Wu "Control and Obstacle Avoidance of Wheeled Mobile Robot" 7th International Conference on Computational Intelligence, Communication Systems and Networks (CICSyN) 978-1-4673-7016-5/15 \$31.00
 © 2015 IEEE